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Thermodynamic (Energy-Exergy) Analysis Of Nine MW Coal Based Thermal Power Plant Using Entropy Generation Principle.

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ABSTRACT: The global concern about energy and fuel cost, environment safety, availability of conventional sources for power generation and fulfillment of energy demand will enhance the adoption of coal &gas based power plants. The rising attention of efficient and resourceful use of energy will support the adopted power generation techniques. The exergy modeling of thermal systems provide the information about, cause of losses, to scale the process, and rectifying the components. In this paper, a thermodynamic analysis of coal based nine MW thermal power plant is carried out. The energy-exergy analysis have been carried out for the boiler, turbine, condenser and pump majorly. The result of thermodynamic analysis is computed in terms of 24.12% plant energy efficiency, 35% of plant exergy efficiency and 11% of boiler energy efficiency respectively. The various exergy destruction in the components have been presented in this paper.

Keywords: Energy-Exergy Analysis, ,Irreversibility Analysis,. Rankine thermal power plant.

I. INTRODUCTION

The large amount of heat is transferred between all utilities of thermal power plant and its greatly affect the plant performance. The First Law of Thermodynamic (FLT) is quantative evaluation of energy, it treat the work and heat interaction with equivalent forms of energy between system and surrounding. The FLT does not provide the information about internal losses, thermal inefficiency due to high grade energy of plant dump in to atmosphere and sustainability. The real performance of thermal system and quality of energy transfer process estimated by the approach of Second Law of Thermodynamic (SLT) called concept of exergy. The term 'Exergy'is maximum possible work obtained from a system at a given state when interacting with a environment, its useful quantity that extract from the SLT. It clearly indicates the inefficiencies of a process by locating the degradation of energy. In short exergy efficiency is true or real efficiency and energy efficiency is approximation of real efficiency. The energy-exergy analysis of 9 MW small size of coal based thermal power unit refers live operational data (Average monthly data of February 2015) of Adani Power Gujrat State of India in present analysis. Major units of plant (boiler, turbines, condensar and pump) have been investigated in proposed thermodynamic model. The main objective of energy-exergy modeling to identifying the magnitude of process, cause of losses and rectifying the components. The numerous researches have been conducted on energy-exergy analysis of various thermal systems, power plant components, and renewable energy conversion systems. Dicer and Rosen [2] stated that, why exergy is important for thermal analysis? They stated that exergy flow rate of a flowing commodity is the maximum rate of work which is obtained from it and it passes reversibly to the environmental state, exchanging heat and materials only with the surroundings. exergy analysis is the theoretical limitations imposed upon a system, clearly pointing out that no real system can conserve exergy and that only a portion of the input exergy can be recovered. Also, exergy analysis quantitatively specifies practical limitations by providing losses in a form in which they are a direct measure of lost exergy.A.Bejan [3] introduced EGM (entropy generation minimization) method, and concluded whenever entropy production is minimized, useful energy is maximized. Khaliq and Kaushik [5] concluded the combustion chamber exergy destruction is 50% of overall exergy destruction of cycle, and effect of intermediate pressure-ratio and effect two stage of reheating on combined GT-ST power cycle performance by using 2nd law thermodynamic approach. Yang et al [6] compared conventional and advanced approach of exergy analysis of supercritical coal thermal power plant. Conventional approach identified exergy destruction of all components, whereas advanced exergyanalysis conclude thermodynamic interactions among thermal utilities for energy saving potential. Ahmadi and Dincer [7] analysed efficiency of dual pressure combined cycle

power plant (CCPP),1st law and 2nd law thermodynamic efficiencies are reduced with the addition of duct burner to HRSG, but power output of CCPP is improved. S.C.Kaushik et al and Aljundi [8,9] review begins with concept of exergy, entropy generation, irreversibility of thermodynamic system and exergy destroyed, and and identify the components having major energy-exergy losses in steam power plant. Gulhane and Thakur [10] investigated amount and source of irreversibilities in 35 TPH capacity of boiler. And also found 76% of exergy destruction at peak load on boiler but 1st and 2nd law efficiency are enhanced. Osueke et al [11] computed maximum exergy destruction 87.3% in boiler, and plant exergy efficiency 11.03% with the effect of water flow in boiler on steam generation and plant output of 75MW of steam power plant, which is located in Sapele-Nigeria. R kumar [12] critically summarized in review of 4-E (energy,exergy,exergonomic and economic) concept for different-different power generation techniques. He addressed the boiler and condenser component have major exergy destruction in case of rankine power cycle, whereas combustion chamber is larger part for exergy destruction in case of gas-turbine power cycle.

II. BRIEF OF STEAM POWER PLANT

The working of coal fired thermal power plant based on Rankine thermal power cycle. The plant size have medium level consisted by major parts 01 boiler unit,03 turbine unit,02 dearators,01 condenser unit, 02 HP heaters,01 pump,etc. Another thermal utilities also provide, the detail of plant layout, dimensions and flow rate values of units are not available due to company privacy policy. The proposed energy-exergy analysis is modeled for major parts of Rankine cycle,boiler,turbines, condenser and pump as per operational data of plant. The plant data is collected in month of February 2015, which is shown in table-1 (a) &(b).

Time	CW FLOW	Temj	perature	Ambient Conditions			Condenser		
		CW - IN	CW - OUT	DBT	RH%	WBT	Vacuum	Temp	Flow
	(m ³ /hr)	(°C)	(°C)	(°C)	(%)	(°C)	(Kg/cm ² g)	(°C)	(TPH)
10:30 AM	2350	29	40	26	57	19.9	-0.93	44.85	15.1
11:00 AM	2350	29	40	28	50	19.9	-0.93	44.96	15.3
11:30 AM	2371	29	40	28	49	19.8	-0.94	43.79	13.9
12:00 PM	2382	29	40	29	47	20.4	-0.94	44.11	14.2
12:30 PM	2383	28.5	40	29	46	20.3	-0.94	43.43	14.3
1:00 PM	2389	28.5	40	28	54	20.8	-0.94	42.13	10.5
1:30 PM	2392	28.5	40	28	54	21.1	-0.94	42.62	11.9
2:00 PM	2382	28.5	40	29	47	20.6	-0.94	43.56	15.1
2:30 PM	2387	28	39	28	46	19.9	-0.94	42.43	12.5

Table-1 (a) Operation data of 9MW steam power plant

Table-1 (b) Operation data of 9MW steam power plant

Time	Inlet Steam		Extra	ction 1 & 2		Extraction 3			
	Pressure (Kg/cm ² g)	Temp (°C)	Flow TPH	Pressure (Kg/cm ² g)	Temp (°C)	Flow TPH	Pressure (Kg/cm ² g)	Temp (°C)	Flow TPH
10:30 AM	61.81	472	68.02	14.21	322.21	15.69	2.53	181.58	39.87
11:00 AM	61.64	473.6	68.90	14.16	324.0	15.46	2.52	183.65	39.94
11:30 AM	62.06	474.4	68.05	14.05	324.0	15.66	2.52	183.60	39.85
12:00 PM	62.31	473.9	67.87	14.03	321.91	14.87	2.52	182.44	39.22
12:30 PM	62.37	472.92	68.54	14.09	321.8	15.33	2.52	182.26	39.72
1:00 PM	61.57	472.96	70.74	14.27	321.8	18.46	2.52	179.84	43.57

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1:30 PM	61.47	477.16	68.74	14.12	328.96	15.53	2.52	186.29	39.72
2:00 PM	61.81	474.09	68.30	14.05	319.08	14.63	2.52	180.03	38.55
2:30 PM	61.77	474.05	70.08	14.28	324.91	16.20	2.52	183.80	41.05

III. ENERGY AND EXERGY ANALYSIS OF NINE MW COAL BASED THERMAL POWER PLANT

All equations of analysis is adopted from fundamental approach of 1^{st} law and 2^{nd} law of thermodynamics, and properties (enthalpy,entropy,specific heat,specific volume,etc) of steam formation referred from steam property table(cited from www.engineeringtoolbox.com/www.spiraxsarco.com) as per steam condition (superheated and saturated) at different pressure-temperature level. PK Nag [1] and Shappiro [4] given energy-exergy equations for power-plant analysis- $\eta_{PLANT} = W_{NET} / Q_{-BOILER}$(1)

$\eta_{\text{PLANT}} = W_{\text{NET}} / Q_{\text{BOILER}} \dots $
$W_{NE} = W_{TURBINETOTAL} - W_{PUMP} \dots \dots$
$W_{\text{TURBINETOTAL}} = W_{\text{TURBINE}_1} + W_{\text{TURBINE}_2} + W_{\text{TURBINE}_3} \dots \dots$
W _{TURBINE_1} =m_dot_turbine1_steamflow(h_temp inlet_turbine1-h_temp exit_turbine1)(4)
W _{TURBINE_2} =m_dot_turbine2_steam flow(h_tempinlet_turbine2-h_temp exit_turbine2)(5)
$W_{\text{TURBINE }3} = \text{m_dot_turbine3_steamflow} (h_\text{temp inlet_turbine3- }h_{2s})(6)$
From enthalpy and entropy balance equation-
$h_{2s}=h_{f2}+x_2h_{fg2}(X2 \text{ is steam dryness fraction at condenser})(7)$
s1=s2s=sf2+x2 sfg2
h1=h_temp inlet_turbine3 = $2827.18 \text{ KJ/Kgtemp}$ at $180 ^{\circ}\text{C}$ (inlet temp of turbine3)
s1=s2 = 7.353 kJ/kg-K from steam properties at condenser line pressure of 0.098 bar (absolute)
h3=hf3=hf2=184 kJ/kg from steam properties
s4=s3=sf2=0.629 kJ/kg-K
hfg2= 2397.95 kJ/kg
sfg2=7.591 kJ/kg-K
Sp Volume of saturated steam at condenser line v=0.001009 m3/kg
Put all values of entropy and get $x^2=0.91$ and estimate h2s from eq. no7
h2s=2376KJ/kg
Now total turbine work (mass flow rate of steam for different turbine provide in plant data table-1
(a)&(b), providing all values of enthalpy as per inlet temperatures Values of turbines)
$W_{\text{TURBINE TOTAL}} = 960 \text{ kJ/kg or } 8.5 \text{ MW}$ (flow rate of steam varying daily with time)
$W_{PUMP} = v \times dP = v \times (P_{BOILERLINE} - P_{CONDENSERLINE}) = m_dot_pump(h4shf3)(9)$
$n_{48} = 184.00 \text{ kJ/kg}$
h4s = 184.06 kJ/kg W _{PUMP} =184 kJ/kg or 437KW at 8.5TPH of water flow through pump
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$W_{PUMP}=184 \text{ kJ/kg or } 437\text{KW at } 8.5\text{TPH of water flow through pump}$ $W_{NET} = 8.2-0.43 = 7.77 \text{ OR } 7.8\text{MW}$ Heat Generated by boiler $Q_{\text{BOILER}}=m_{\text{dot}}\text{boilersteamflow (h_boiler temp - h4s)}(10)$
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$\begin{split} W_{\text{PUMP}} = & 184 \text{ kJ/kg or } 437 \text{KW at } 8.5 \text{TPH of water flow through pump} \\ W_{\text{NET}} = & 8.2 \text{-} 0.43 = 7.77 \text{ OR } 7.8 \text{MW} \\ \text{Heat Generated by boiler} \\ Q_{\text{BOILER}} = & \text{m_dot_boilersteamflow (h_boiler temp - h4s)}(10) \\ & (\text{Steam flow through boiler is } 65 \text{TPH from data table}) \\ Q_{\text{BOILER}} = & 3196 \text{ kJ/kg or } 58627 \text{ KW} \\ & \text{For } Q_{\text{CONDENSER}} \dots W_{\text{TURBINE TOTAL}} - W_{\text{PUMP}} = & Q_{\text{BOILER}} - & Q_{\text{CONDENSER}}(11) \\ & \Box_{\text{PLANT}} = & W_{\text{NET}} / & Q_{\text{BOILER}} = 24.12\% \end{split}$
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$W_{PUMP}=184 \text{ kJ/kg or } 437\text{KW at } 8.5\text{TPH of water flow through pump}$ $W_{NET} = 8.2-0.43 = 7.77 \text{ OR } 7.8\text{MW}$ Heat Generated by boiler $Q_{_BOILER}=m_{_dot_boilersteamflow (h_boiler temp - h4s)(10)}$ (Steam flow through boiler is 65TPH from data table) $Q_{_BOILER} = 3196 \text{ kJ/Kg or } 58627 \text{ KW}$ For $Q_{_CONDENSER}$ $W_{\text{TURBINE TOTAL}} - W_{\text{PUMP}} = Q_{_BOILER} - Q_{_CONDENSER}$ (11) $\Box_{\text{PLANT}} = W_{\text{NET}} / Q_{_BOILER} = 24.12\%$ $\eta_{\text{Boiler}} = Q_{_BOILER} / Q_{_FUEL}$ $Q_{_FUEL} = (m_{_air} + m_{_fuel}) \times \text{fuel calorific value}$ (12) $\Box_{\text{Boiler}} = 11\%$ (13 TPH of coal feeding with 97 TPH of air) Exergy flow rate of inlet steam- $\varepsilon_{f_ln} = m_{_dot_steam} \times \text{cp_boiler steam} \times \text{To} \left[\frac{\text{Tboiler}}{T_0} - 1 - ln \frac{\text{Tboiler}}{T_0}\right]$ (13)
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$\begin{split} & W_{\text{PUMP}} = 184 \text{ kJ/kg or } 437 \text{KW at } 8.5 \text{TPH of water flow through pump} \\ & W_{\text{NET}} = 8.2 \text{-} 0.43 = 7.77 \text{ OR } 7.8 \text{MW} \\ & \text{Heat Generated by boiler} \\ & Q_{_BOILER} = \text{m_dot_boilersteamflow (h_boiler temp - h4s)}(10) \\ & (\text{Steam flow through boiler is } 65 \text{TPH from data table}) \\ & Q_{_BOILER} = 3196 \text{ kJ/Kg or } 58627 \text{ KW} \\ & \text{For } Q_{_CONDENSER} \dots W_{\text{TURBINE TOTAL}} - W_{\text{PUMP}} = Q_{_BOILER} - Q_{_CONDENSER}(11) \\ & \Box_{\text{PLANT}} = W_{\text{NET}} / Q_{_BOILER} = 24.12\% \\ & \eta_{\text{Boiler}} = Q_{_BOILER} / Q_{_FUEL} \\ & Q_{_FUEL} = (m_air + m_fuel) \times \text{fuel calorific value}(4620 \text{ kcal/kg as per data})(12) \\ & \Box_{\text{Boiler}} = 11\% \\ & (13 \text{ TPH of coal feeding with } 97 \text{ TPH of air}) \\ & \text{ExergyBalance Equation-} \\ & \text{Exergy flow rate of inlet steam} \\ & \notin_{\underline{f}_1n} = m_dot_steam \times \text{cp_boiler steam} \times \text{To } [\frac{\text{Tboiler}}{\text{To}} - 1 - \ln \frac{\text{Tboiler}}{\text{To}}](13) \\ & (\text{Steam generation inlet temperature is } 485 \pm 5^{0}\text{C}, 75\text{TPH} \text{ and specific heat of steam } 2.21 \text{ kJ/kg-k, atmospheric temp To is } 298\text{K}) \\ \end{aligned}$
$W_{PUMP}=184 \text{ kJ/kg or } 437\text{KW at } 8.5\text{TPH of water flow through pump}$ $W_{NET} = 8.2-0.43 = 7.77 \text{ OR } 7.8\text{MW}$ Heat Generated by boiler $Q_{_BOILER}=m_{_}\text{dot_boilersteamflow (h_boiler temp - h4s)}(10)$ (Steam flow through boiler is 65TPH from data table) $Q_{_BOILER} = 3196 \text{ kJ/kg or } 58627 \text{ KW}$ For $Q_{_CONDENSER} \dots W_{\text{TURBINE TOTAL}} - W_{\text{PUMP}} = Q_{_BOILER} - Q_{_CONDENSER}(11)$ $\Box_{\text{PLANT}} = W_{\text{NET}} / Q_{_BOILER} = 24.12\%$ $\eta_{\text{Boiler}} = Q_{_BOILER} / Q_{_FUEL}$ $Q_{_FUEL} = (m_air + m_fuel) \times \text{fuel calorific value}(4620 \text{ kcal/kg as per data})(12)$ $\Box_{\text{Boiler}} = 11\%$ (13 TPH of coal feeding with 97 TPH of air) Exergy Balance Equation- Exergy flow rate of inlet steam- $\varepsilon_{f_ln} = m_dot_steam \times \text{cp_boiler steam} \times \text{To} \left[\frac{^{Tboiler}}{_{To}} - 1 - ln \frac{^{Tboiler}}{_{To}}\right](13)$ (Steam generation inlet temperature is $485 \pm 5^{\circ}$ C, 75TPH and specific heat of steam 2.21 kJ/kg-k , atmospheric temp To is 298K) $\varepsilon_{f_ln} = 387 \text{ kJ/Kg or }7715\text{KW}$
$\begin{split} & W_{\text{PUMP}} = 184 \text{ kJ/kg or } 437\text{KW at } 8.5\text{TPH of water flow through pump} \\ & W_{\text{NET}} = 8.2-0.43 = 7.77 \text{ OR } 7.8\text{MW} \\ & \text{Heat Generated by boiler} \\ & Q_{_BOILER} = \texttt{m_dot_boilersteamflow (h_boiler temp - h4s)}(10) \\ & (\text{Steam flow through boiler is } 65\text{TPH from data table}) \\ & Q_{_BOILER} = 3196 \text{ kJ/Kg or } 58627 \text{ KW} \\ & \text{For } Q_{_CONDENSER} \dots \text{ W}_{\text{TURBINE TOTAL}} - \text{W}_{\text{PUMP}} = Q_{_BOILER} - Q_{_CONDENSER} \dots (11) \\ & \Box_{\text{PLANT}} = W_{\text{NET}} / Q_{_BOILER} = 24.12\% \\ & \eta_{\text{Boiler}} = Q_{_BOILER} / Q_{_FUEL} \\ & Q_{_FUEL} = (\texttt{m_air} + \texttt{m_fuel}) \times \text{fuel calorific value} \dots (4620 \text{ kcal/kg as per data}) \dots (12) \\ & \Box_{\text{Boiler}} = 11\% \\ & (13 \text{ TPH of coal feeding with 97 TPH of air}) \\ & \text{Exergy flow rate of inlet steam-} \\ & \varepsilon_{f_1n} = \texttt{m_dot_steam} \times \texttt{cp_boiler steam} \times \text{To } [\frac{\texttt{Tboiler}}{\texttt{To}} - 1 - ln\frac{\texttt{Tboiler}}{\texttt{To}}] \dots (13) \\ & (\text{Steam generation inlet temperature is } 485 \pm 5^{0}\text{C}, 75\text{TPH and specific heat of steam } 2.21 \text{ kJ/kg-k, atmospheric temp To is } 298\text{K}) \\ & \varepsilon_{f_1n} = 387 \text{ kJ/Kg or } 7715\text{KW} \\ & \text{Exergy flow rate of exhaust steam-} \end{aligned}$
$W_{PUMP}=184 \text{ kJ/kg or } 437\text{KW at } 8.5\text{TPH of water flow through pump}$ $W_{NET} = 8.2-0.43 = 7.77 \text{ OR } 7.8\text{MW}$ Heat Generated by boiler $Q_{_BOILER}=m_{_}\text{dot_boilersteamflow (h_boiler temp - h4s)}(10)$ (Steam flow through boiler is 65TPH from data table) $Q_{_BOILER} = 3196 \text{ kJ/kg or } 58627 \text{ KW}$ For $Q_{_CONDENSER} \dots W_{\text{TURBINE TOTAL}} - W_{\text{PUMP}} = Q_{_BOILER} - Q_{_CONDENSER}(11)$ $\Box_{\text{PLANT}} = W_{\text{NET}} / Q_{_BOILER} = 24.12\%$ $\eta_{\text{Boiler}} = Q_{_BOILER} / Q_{_FUEL}$ $Q_{_FUEL} = (m_air + m_fuel) \times \text{fuel calorific value}(4620 \text{ kcal/kg as per data})(12)$ $\Box_{\text{Boiler}} = 11\%$ (13 TPH of coal feeding with 97 TPH of air) Exergy Balance Equation- Exergy flow rate of inlet steam- $\varepsilon_{f_ln} = m_dot_steam \times \text{cp_boiler steam} \times \text{To} \left[\frac{^{Tboiler}}{_{To}} - 1 - ln \frac{^{Tboiler}}{_{To}}\right](13)$ (Steam generation inlet temperature is $485 \pm 5^{\circ}$ C, 75TPH and specific heat of steam 2.21 kJ/kg-k , atmospheric temp To is 298K) $\varepsilon_{f_ln} = 387 \text{ kJ/Kg or }7715\text{KW}$

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(Steam temperatureexhaust is 320 °C, 75TPH and specific heat of steam 2.21 kJ/kg-k, atmospheric temp To is 298K)
Rate of exergy decrease- $\oint_{f_{ln}} \oint_{f_{out}} = 127 \text{ KJ/Kg or } 2475 \text{ KW}$ (15)
Rate of exergy loss during steam generation= $\frac{\text{Ef_out}}{\text{Ef_in}} = 0.47$ (16)
Rate of exergy increase of steam = Exergyutilization rate = $\bigoplus_{f_Usefull}$
Exergy Destruction in boiler= $\in_{\text{Des}_{boiler}}$ = Rate of exergy increase of steam - Rate of exergy decrease
Exergy flow rate of wet steam to condenser
(26THP of wet steam passing through condenser) $f = 188.25 K I/K \alpha \text{ or } 1250.44 KW$
€ _{wet steam to condenser} = 188.25 KJ/Kg or 1350.44 KW Irreversibility estimation of each components-
$I_{RR} = To\Sigma\Delta S = To (\Delta S_{boiler} + \Delta S_{turbine} + \Delta S_{condenser} + \Delta S_{pump}).$ (19)
And $\Delta S = cpln(\frac{Tout}{\tau in})$ from 2 nd law of thermodynamics
(cp will vary with temperature and pressure condition of working fluid, putting all value of cp and Tout&Tin of
components)
$I_{RR_Boiler} = To(\Delta S)_boiler} = 1086 \text{ KJ/Kg}$
$I_{RR_turbine} = To(\Delta S)_turbine = 419 \text{ KJ/Kg}$
$I_{RR_condenser} = To(\Delta S)\{cond} = 124 \text{ KJ/Kg}$
$I_{RR_pump} = 10(\Delta S)_{pump} = 01.17 \text{ KJ/Kg}$
$I_{RR_pump} = To(\Delta S)\{pump} = 61.17 \text{ KJ/Kg}$ Now EDR ratio = $\frac{To\Sigma\Delta S}{Qboiler}$ (21)
EDR ratio = 0.65
Exergetic efficiency = η_{EX} = 1- EDR _{ratio} (22)
$\Box_{\text{EX}} = 1 - \text{EDR}_{\text{ratio}} = 0.35$
Exergy Destruction Rate = $\frac{To \Sigma \Delta S}{Wnet}$
Exergy Destruction Rate = 2.73
Exclose Destruction Factor = 2.75

IV. RESULT AND DISCUSSION

The property of steam of parts of plant is taken from steam property chart with variation of pressuretemperature and saturated & superheated state of steam condition as per available data. All values of enthalpy, entropy and specific heat shown in table -2 to Table-5 respectively.

	ŗ	Fable-2 Boiler	Observation		
Pressure	Temp	Flow	Enthalpy	Entropy	Sp Heat
(Kg/cm ² gauge)	(°C)	(Kg/s)	(kJ/Kg)	(kJ/Kg-K)	(kJ/Kg-K)
61.81	472	18.89	3353.1	6.7778	2.418
61.64	473.6	19.10	3357.32	6.7848	2.415
62.06	474.4	18.9	3358.73	6.7838	2.416
62.31	473.9	18.85	3337.13	6.7796	2.418
62.37	472.92	19.05	3354.68	6.7759	2.42
61.57	472.96	19.65	3355.9	6.7836	2.415
61.47	477.16	19.09	3366.17	6.7981	2.409
61.81	474.09	18.97	3358.23	6.7841	2.415
61.77	474.05	19.46	3358.7	6.7851	2.415
61.87	473.90	19.11	3357.69	6.7833	2.416

				o condenis		acron			
Vacuum Pr	Temp	Flow	Enthalpy (KJ/Kg)		Entropy (KJ/Kg-k)			Sp Heat	
(Kg/cm ² gauge)	(°C)	(kg/s)	$\mathbf{h}_{\mathbf{f}}$	\mathbf{h}_{gf}	hg	S_{f}	S_{fg}	S_{g}	(kJ/Kg-K}
-0.934	44.85	4.2	164.9	1866.9	2031.8	0.554	5.772	6.326	1.505
-0.933	44.96	4.25	166.6	1885.9	2052.6	0.559	5.831	6.391	1.52
-0.937	43.79	3.35	159.9	1809.7	1969.6	0.553	5.595	6.133	1.459
-0.936	44.11	3.94	161.6	1828.8	1990.4	0.542	5.654	6.197	1.474
-0.939	43.43	3.98	148.1	1771.1	1928.2	0.526	5.478	6.004	1.351
-0.944	42.13	2.92	153.1	1676.1	1824.5	0.497	5.183	5.68	1.397
-0.941	42.62	3.3	159.1	1733.5	1886.7	0.514	5.36	5.874	1.549
-0.937	43.56	4.2	151.5	1809.5	1969.6	0.537	5.595	6.133	1.382
-0.942	42.43	3.48	154.8	1714.5	1866	0.509	5.301	5.18	1.412
-0.94	43.54	3.74	154.8	1752.6	1907.4	0.52	5.419	5.939	1.551

Table-3 Condenser observation

Table-4 Turbine 1& 2 Observation

Pressure	Тетр	Flow	Enthalpy	Entropy	Sp Heat
(Kg/cm ² gauge)	(°C)	(Kg/s)	(kJ/Kg)	(kJ/Kg-K)	(kJ/Kg-K)
14.21	322.21	4.35	3086.33	7.0028	2.202
14.16	324.0	4.29	3090.39	7.0111	2.2
14.05	324.0	4.35	3080.65	7.0148	2.116
14.03	321.91	4.15	3086.14	7.007	2.2
14.09	321.8	4.25	3085.7	7.005	2.201
14.27	321.8	5.12	3085.28	6.999	2.204
14.12	328.96	4.31	3101.38	7.03	2.195
14.05	319.08	4.06	3079.82	6.996	2.203
14.28	324.91	4.50	3092.11	7.01	2.201
14.14	323.19	4.38	3088.65	7.008	2.2

Table-5 Turbine-3 Observation

Pressure	Temp	Mass Flow Rate	Enthalpy	Entropy	Sp Heat
(Kg/cm ² gauge)	(°C)	Kg/s	kJ/Kg	kJ/Kg-K	kJ/Kg-K
2.53	181.58	11.07	2824.18	7.153	2.097
2.52	183.65	11.09	2828.67	7.164	2.093
2.52	183.60	11.06	2828.57	7.164	2.093
2.52	182.44	11.03	2826.14	7.159	2.095
2.52	182.26	11.03	2825.76	7.158	2.095
2.52	179.84	12.1	2820.69	7.147	2.099
2.52	186.29	11.03	2834	7.178	2.089
2.52	180.03	10.7	2821.09	7.147	2.099
2.52	183.80	11.4	2822.7	7.151	2.098
2.52	182.61	11.17	2826.5	7.159	2.095

The numerical computation of nine MW coal based thermal power plant is carried out and performance parameters in terms of plant efficiency boiler efficiency, exergetic efficiency of plant and irreversibilities in terms of exergy destruction in various components, exergy destruction ratio of plant is shown in table-respectively.

Table-6 Parametric	Result
Thermodynamics Parameters	Computed Results
Net Out Put (Wnet)	7.8MW
Total Turbine Out Put (Wturbine)	8.5 MW
Boiler Heat Generation (Qboiler)	3196KJ/KG
Plant Efficiency (\Box_{PLANT})	24.12&
Boiler Efficiency (BOILER)	11%
Plant Exergy Destruction Rate	2.17
Plant Exergetic Efficiency (CEXERGY)	35%

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V. CONCLUSIONS & RECOMMENDATION

The exergy analysis plays deterministic role in identifying the magnitude of thermodynamic processes, cause of losses and rectifying the exergy destruction rate in the components due to energy saving in components (i.e.boilers, condensers in steam power plant)

- 1. The maximum exergy destruction(irreversibility) as 34%.
- Exergy Destruction is found to be 2.17 (which is the based on output analysis) and 0.65 based on input. 2.
- 3. The plant efficiency is 24.12%
- 4. The second law efficiency is 35%

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REFERENCES

- [1]. P.K Nag,"Power Plant Engineering"Tata McGraw Hill, New Delhi, 2007.
- M.A.Rosen and I. Dincer" Exergoeconomic analysis of power plants operating on various fuels" Applied Thermal Engineering, 23, pp [2]. 643-658,2003.
- A.Bejan "Fundamentals of ExergyAnalysis, EntropyGeneration, Minimization and Generation of Flow Architecture" International [3]. Journal of Energy Research, Vol, 26, No.7, 2002, pp545-565.
- [4]. MichealJ.Moran and Howard N.Shapiro "Fundamentals of Engineering Thermodynamics" 6th edition, SI Version, John Willey & Sons, Corporation, 2010.
- [5]. Khaliq and S.C Kaushik "Second-law based thermodynamic analysis of brayton/rankine combined power cycle with reheat" Applied Energy, Vol 78, No.2, pp 179-197, 2004.
- [6]. Y.Yang,L.Wang,C.Dong,G.Xu,T.Morousk and G.Tsatsaronis "Comprehensive exergy based evaluation and parametric study of a coal-fired ultra supercritical powerplant". Applied Energy, 2013.
- [7]. P.AhmadiandI.Dincer"Thermodynamic analysis and Thermoeconomic optimization of a dual pressure combined cycle power plant with supplementary firing unit"Energy Conversion Management, 52, pp 2296-308, 2011
- [8]. S.C Kaushik, V.S.Reddy and S.K Tyagi "Energy and Exergy analysis of thermal power plants-A Review"Renewable and Sustainable Energy Reviews, 15, pp 1857-1872, 201.
- I.H. Aljundi"Energy and exergy analysis of a steam power plant in Jordan" Applied Thermal Engineering, 29, pp 324-328, 2009. [9].
- [10]. Sarang J Gulhane, Amitkr Thakur "Exergy analysis of boiler in cogeneration thermal power plant" Americal journal of engineering research,e-issn-2320-0847,p-issn-2320-0936,vol-02,issue-10,pp-385-392,2013.
- [11]. Christian O.Osueke, Anthony O. Onokwai and AdeyinkaO.Adeoye "Energy and exergy analysis of 75 MW steam power plant in Sapele (Nigeria) "International journal of innovative research in advanced engineering ISSN-2349-2163,vol-2,issue-6,pp-169-179,2015
- [12]. Ravindra kumar "A critical review on energy, exergo, exergonomics and economic (4-E) analysis of thermal power plants" Engineering Science and Technology, an International Journal, Elsevier, issn-2215-0986, pp 283-292, Feb 2017.

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